



# Reliability of Dynamic Simulation to reproduce plant dynamics

Repsol – Inprocess

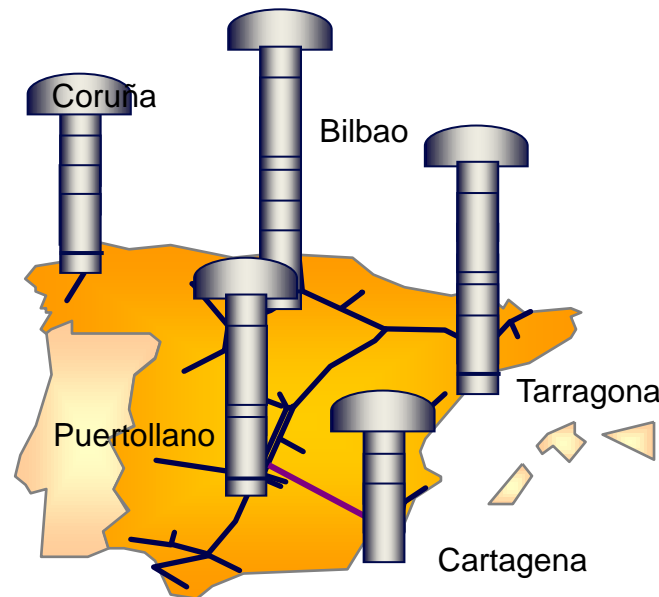
Manel Serra (Inprocess), JoseMaria Ferrer (Inprocess), Jose Garcia Vega (Repsol Tarragona Refinery), Francisco Cifuentes (Repsol Refining APC) , Marta Yugo and Maria Luisa Suarez (Repsol Technology Center)

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# Repsol Presentation

- Integrated company: upstream, downstream, petrochemicals, gas
- Repsol downstream activities regionally based in Europe and South-America.
- Repsol has 6 refineries, 5 in Spain and 1 in Peru
- It is the refining leader in Iberia and the third LPG company in the world.
- Spanish refineries process 0.9 million bbl/day



# Agenda

- Simulation: What is, Why and How good
- Case Study: Double C3Splitter
- Ideas for Future

# What is Process Simulation

From time to time someone tells me:

“ I don't believe in process simulation”

Well... that's like saying:

“ I don't believe in the Bernoulli equation”

Simulation is not a question of believing or not believing

Process simulation is only a macro-  
compilation of physics, chemistry and  
thermodynamics laws smartly coded  
in an interactive computer application.

Just a megaprocesscalculator.



1600 1700 1800 1900 2000

Chemistry, Mathematics, Physics

- 1614: Napier Logarithms
- 1637: Descartes Cartesian geo
- 1662: Boyle's Gas Law
- 1665: Calculus (Leibniz)
- 1669: Newton's Method
- 1680: Algebraic logic Leibniz
- 1687: Newton's Motion and Cooling

- 1738: Bernoulli's Law
- 1760: Lambert's Law
- 1768: Euler's Method
- 1785: Coulomb's Law
- 1785: Laplace's transform
- 1787: Charles's Gas Law
- 1791: Richter's reaction Law

- 1801: Dalton's Law Partial P.
- 1802: Henri's Gas Law
- 1808: Gay-Lussac's Law
- 1811: Avogadro's Gas Law
- 1822: Fourier's Heat Law
- 1823: F.T. Calculus (Cauchy)
- 1829: Graham's Effusion Law
- 1831: Faraday's Electrolysis
- 1840: Hess's Enthalpy Law
- 1840: Poiseuille's Flow Law
- 1850: Clausius's Law Thermo.
- 1851: Stoke's Viscosity Law
- 1852: Beer's Absortion Law
- 1854: Boolean Algebra
- 1855: Fick's Diffusion Laws
- 1864: Kopp's Heat Cap. Law
- 1866: Maxwell's Gas Viscosity
- 1869: Mendeleyev's Periodic
- 1871: Coppet's Freezing Point
- 1871: Boltzmann's Distribut. L
- 1873: EO Van der Waals
- 1882: Raoult's Vapor Pressure
- 1885: van't Hoff's Osmotic Pr.
- 1893: Sutherland's Gas Visco.

- 1900: Planck's Raditon Law
- 1908: Grüneisen's Thermal L.
- 1913: Heisenberg principle
- 1923: Pauli's Exclusion prin.
- 1925: Fermi-Dirac distribution
- 1949: EO Redlich-Kwong
- 1972: EO Soave R-K
- 1976: EO Peng-Robinson
- 1999: EO Elliot-Suresh-Donoh.

This science has been there long time ago, but we are the first generation of people who has in our hands software tools and desktop computers capable to simulate dynamically entire process units.

Most of their applications are still in the early stages

- 1200: Abacus
- 1621: Slide Rule
- 1673: Leibniz's Step Reckoner

1700

- 1801: Punched Cards
- 1822: Mechanical Computer (Babbage)
- 1879: Cash Register (Ritty)

- 1930: Mechanical calculator
- 1934: Differential Analyzer
- 1939: Turing decrypter
- 1st Generation**
- 1946: ENIAC
- 1952: IBM 701
- 2nd Gen.: transistor**
- 1959: IBM 1401
- 3rd Gen.: integrated circuit**
- 1964: IBM System/360
- 4th Gen.: Microprocessor**
- 1971: Intel 4004
- 1977: VAX-11/780
- 1978: Intel 8086
- 1980: Sinclair ZX80
- 1982: Intel 80286, 1985: Intel 80386, 1989: Intel 80486
- 1993: Intel Pentium
- 2006: Intel Core line
- 2010: Intel Core i3,i5,i7

Computers

# Why Dynamic Simulation

- Consolidated
- Exploring

## 1.- Equipment sizing and process layout verification:

- Compression systems
- Pipeline networks

## 2.- Flare Load calculation and PSV sizing

- Design/revamp flare networks

## 3.- Emergency System verification and HAZOP studies support

- HIPPS studies
- Cause & Effect matrixes

## 4.- Design control layout

- Scenarios analysis
- Perturbation rejection
- Control loops selection

## 6.- Develop virtual sensors

- Online Analyzers backup
- Fault diagnostic
- Look-ahead sensors

## 7.- DCS checkout

- DCS FAT with virtual plant
- Operating procedure test

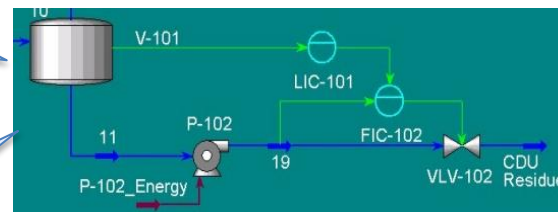
## 8.- Operator Training System(OTS)

- Operator Training
- Emergency scenarios
- Knowledge base system

## 5.- Prototyping MPC

- Obtain MPC models
- Study non-linearities
- Test/Tune MPC controller

### Dynamic Model



# How good are the models

Well... plants are built based in steady-state models (they should be good enough)

But when moving to Dynamics, how good are they?

If the plant is being built there is no way to know it. You have to trust in the tool and the experience of the modeler

If the plant is available there are three methods:

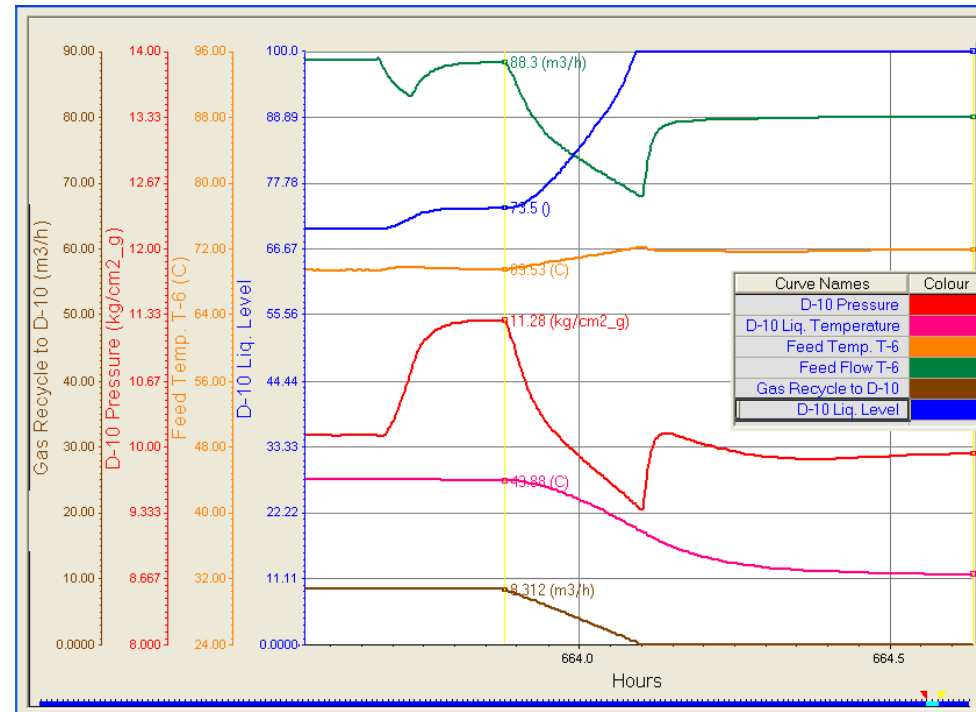
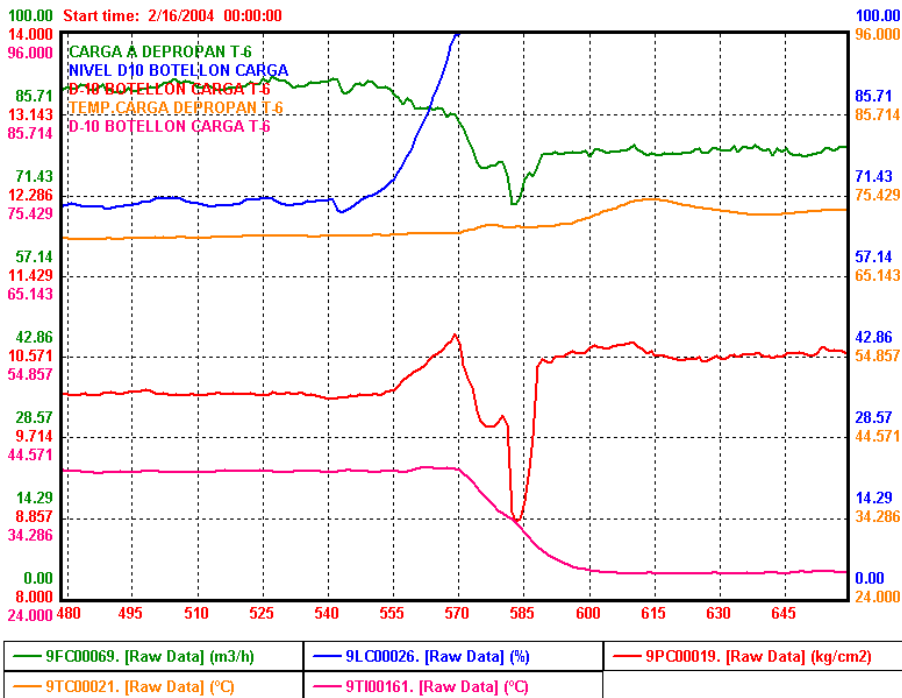
1. Compare responses of single moves
2. Compare DMCplus models (plant vs. model)
3. Feed historical data into the model (presented here)

# Method 1: Single moves

Shown in a debutanizer in AspenTech ACO UGM 2005 Barcelona

Real Plant

HYSYS Dynamics

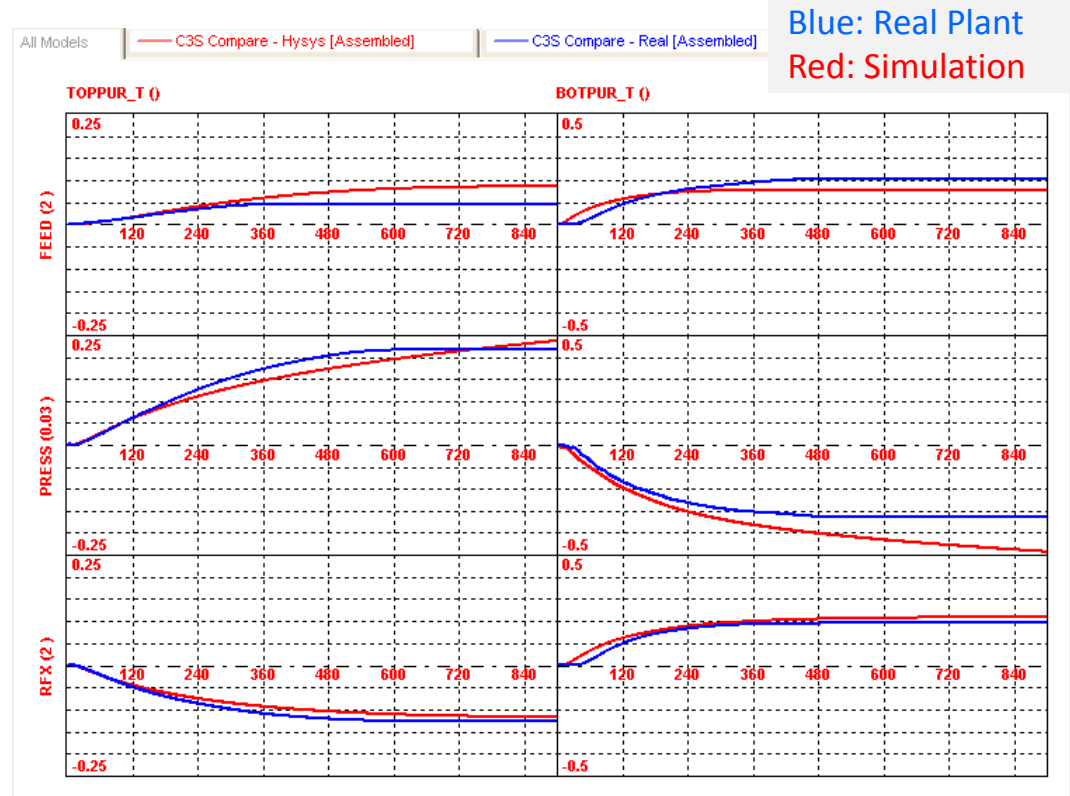
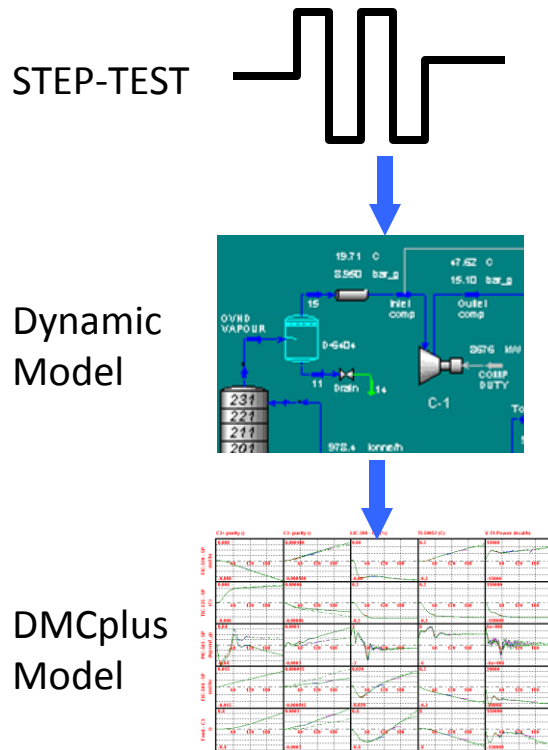


Reference: [www.aspentech.com/publication\\_files/HP0906\\_Gonzalez\\_PDF.pdf](http://www.aspentech.com/publication_files/HP0906_Gonzalez_PDF.pdf)



# Method 2: DMCplus models

Shown in a C3 Splitter in AspenTech UGM 2008 Berlin (APC track)



Other References:

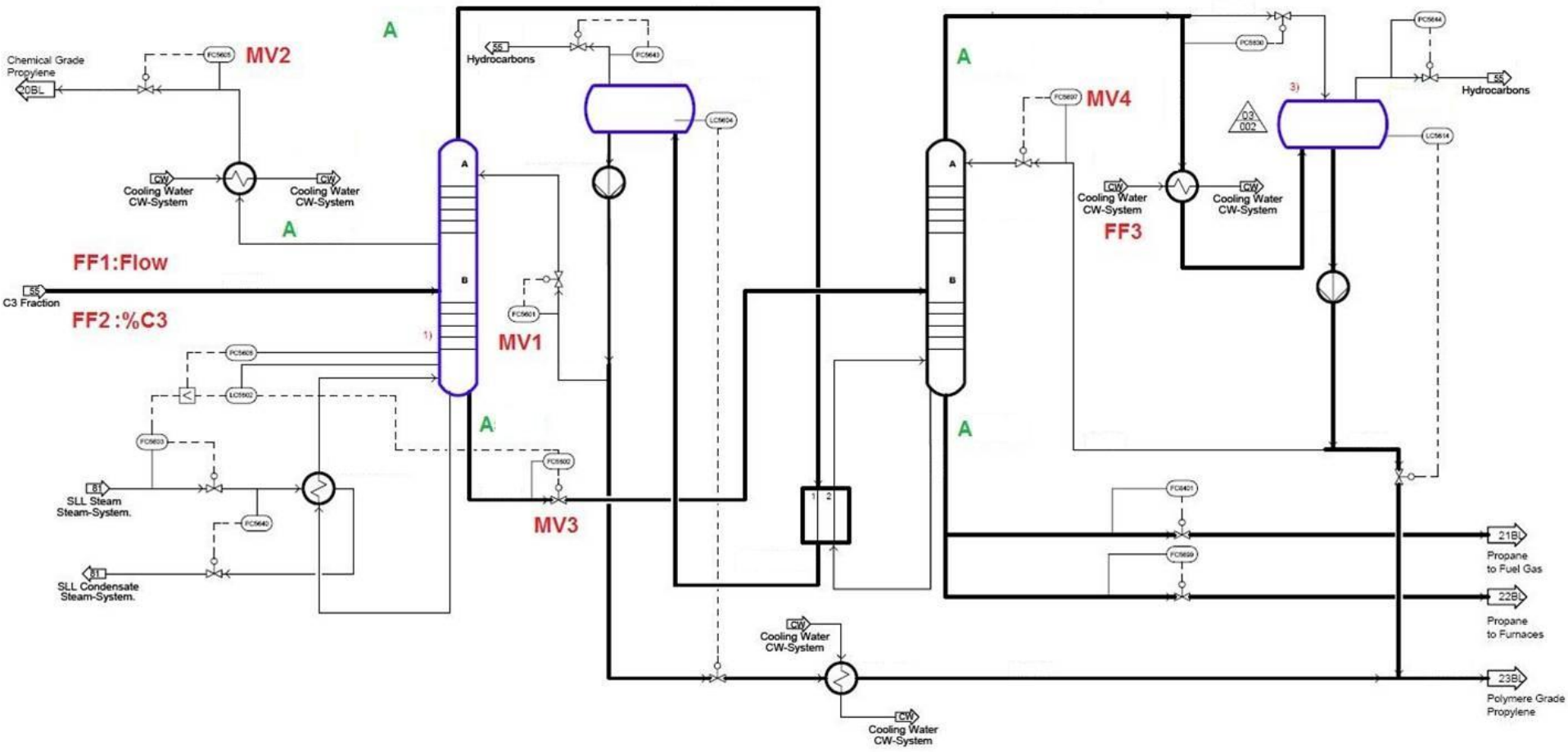
1. [www.aspentech.com/publication\\_files/Hydrocarbon\\_Engineering\\_Nov\\_2004.pdf](http://www.aspentech.com/publication_files/Hydrocarbon_Engineering_Nov_2004.pdf)
2. [www.aspentech.com/workarea/downloadasset.aspx?id=6442451960](http://www.aspentech.com/workarea/downloadasset.aspx?id=6442451960)

# Double C3 splitter polymer grade

1<sup>st</sup> column: 189 trays, lateral extraction chemical grade

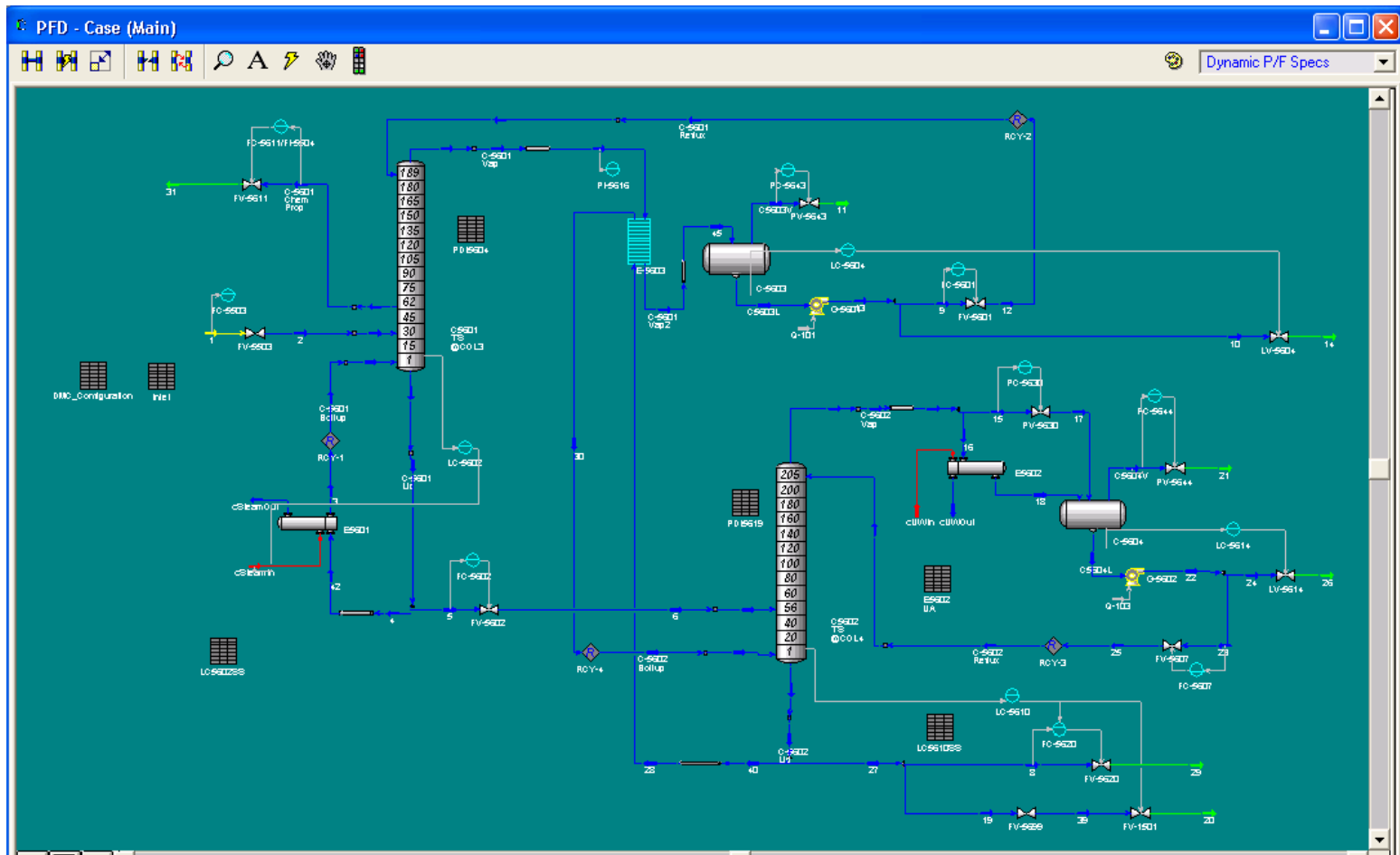
2<sup>nd</sup> column: 205 trays, reboiler is condenser of 1<sup>st</sup> column

Challenging to control: very long settling times, heat interaction, external disturbances and intrinsic non-linearity

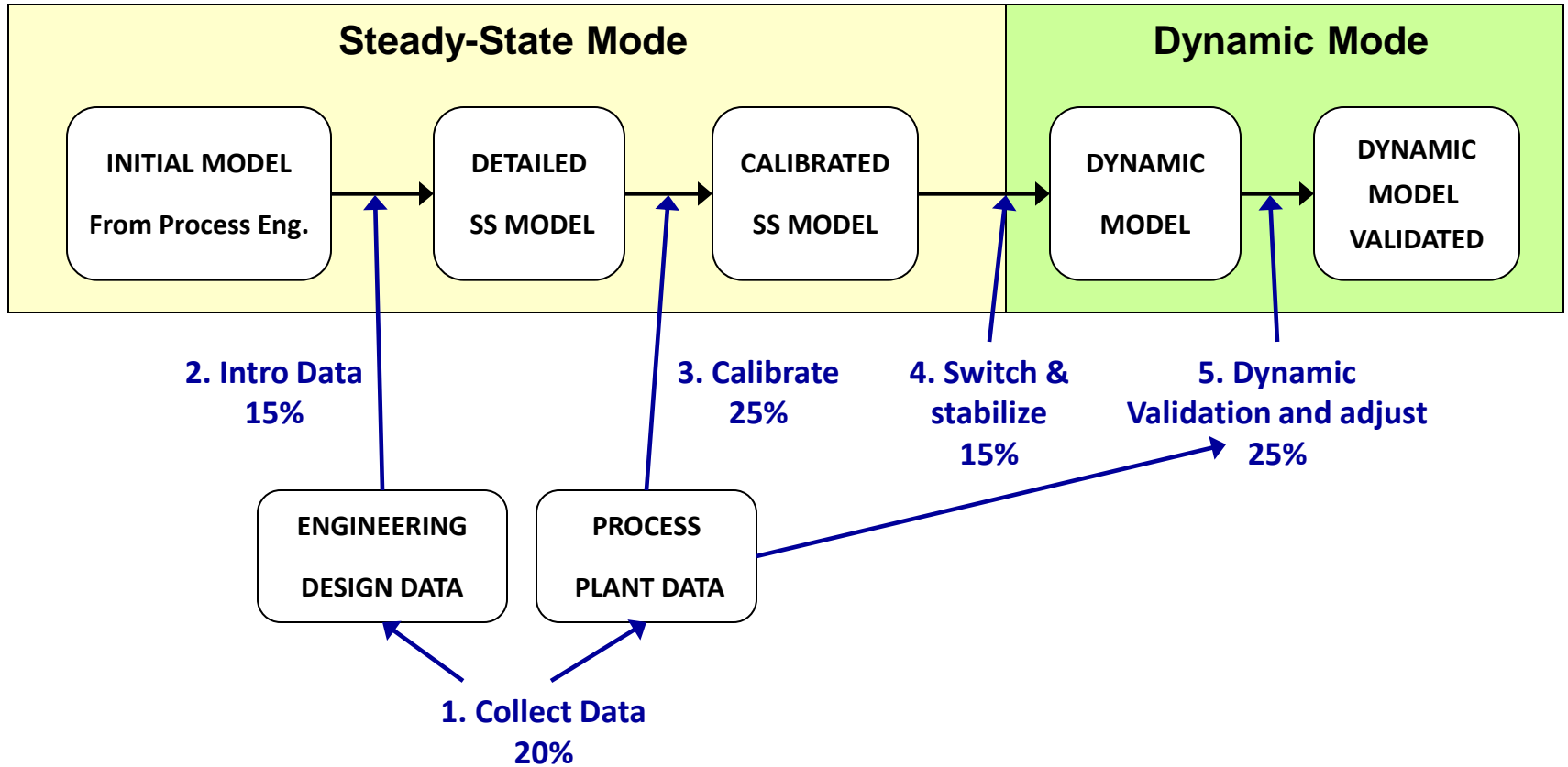


# HYSYS Dynamics model

A HYSYS Dynamics model integrated with a DMCplus controller was developed in order to analyze unit interactions and dynamics, change basic regulatory controllers, generate HYSYS based DMC model and train engineers on their use.



# Model Building steps

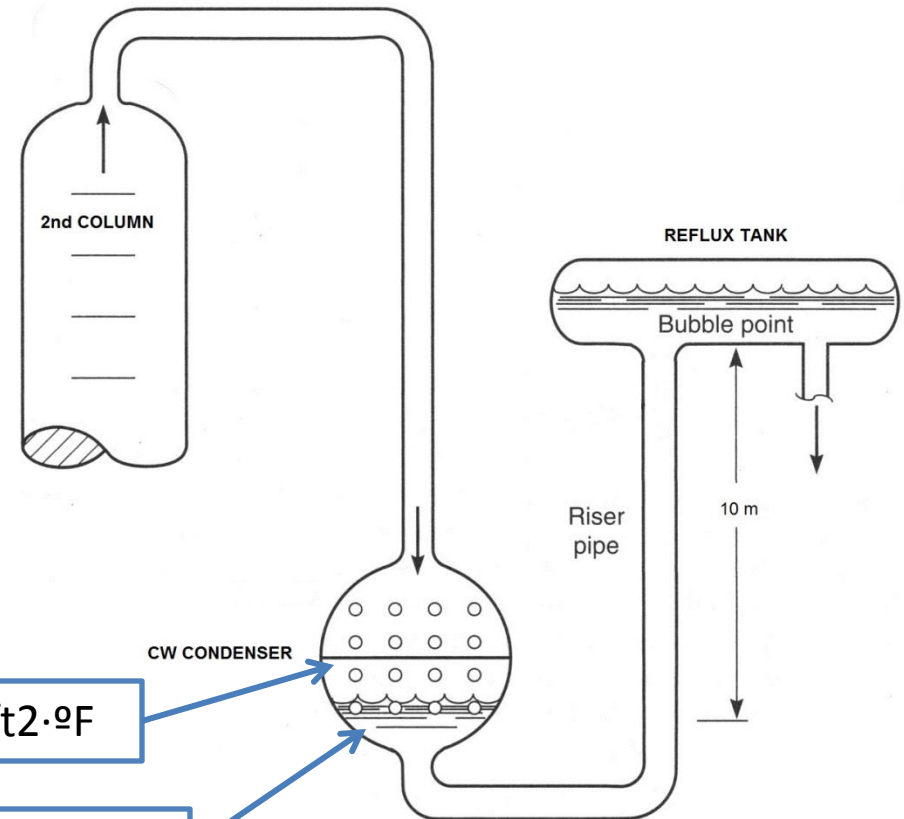


Percentages are efforts required for the model building

# Self regulated top pressure

The liquid level in the shell depends on the differential pressure between top and reflux tank.

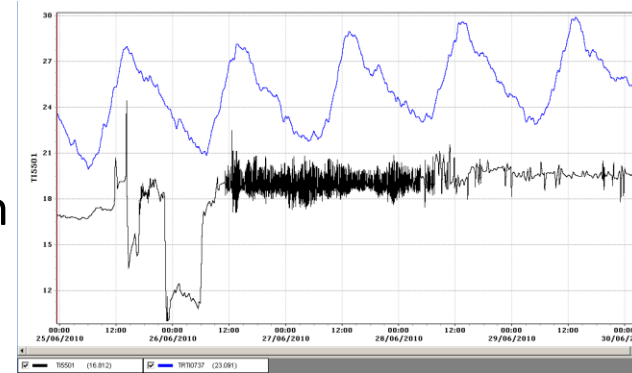
Heat transfer coefficient ( $U$ ) of the 2<sup>nd</sup> column condenser fully depends on the liquid level in the shell side.



U Condensing Zone: 400 – 1000 Btu/h·ft<sup>2</sup>·°F

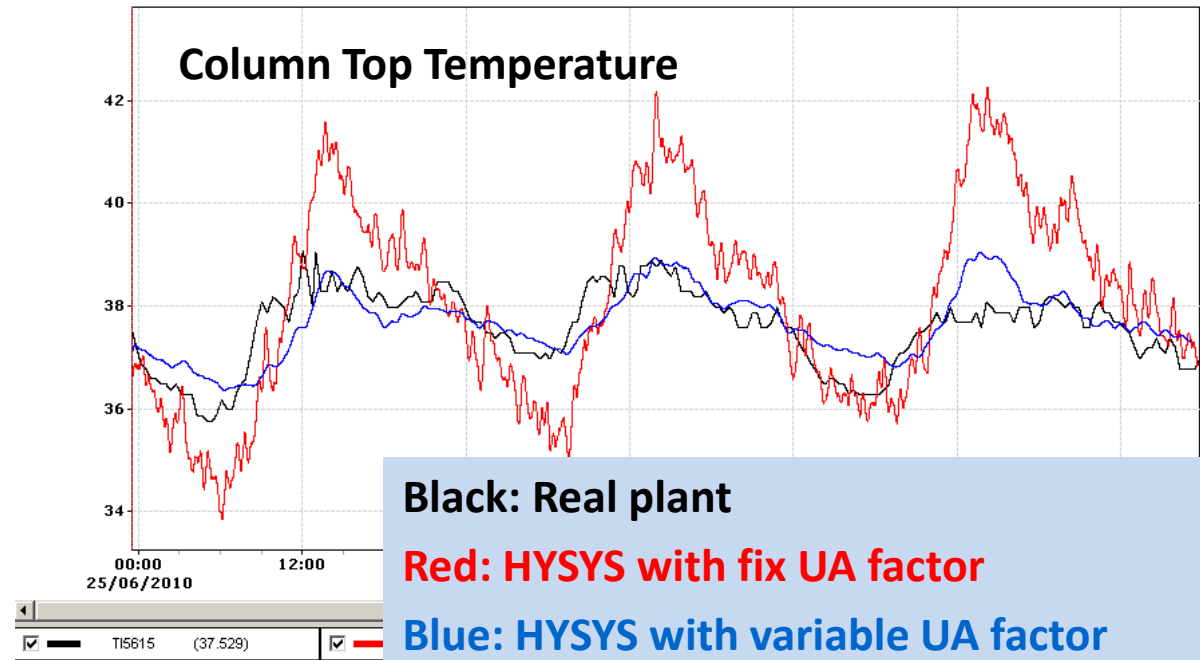
U Subcooling Zone: 10 – 30 Btu/h·ft<sup>2</sup>·°F

Changes in the Cooling Water temperature (day/night) affects to the condenser duty and hence to the column top pressure and condenser shell liquid level.

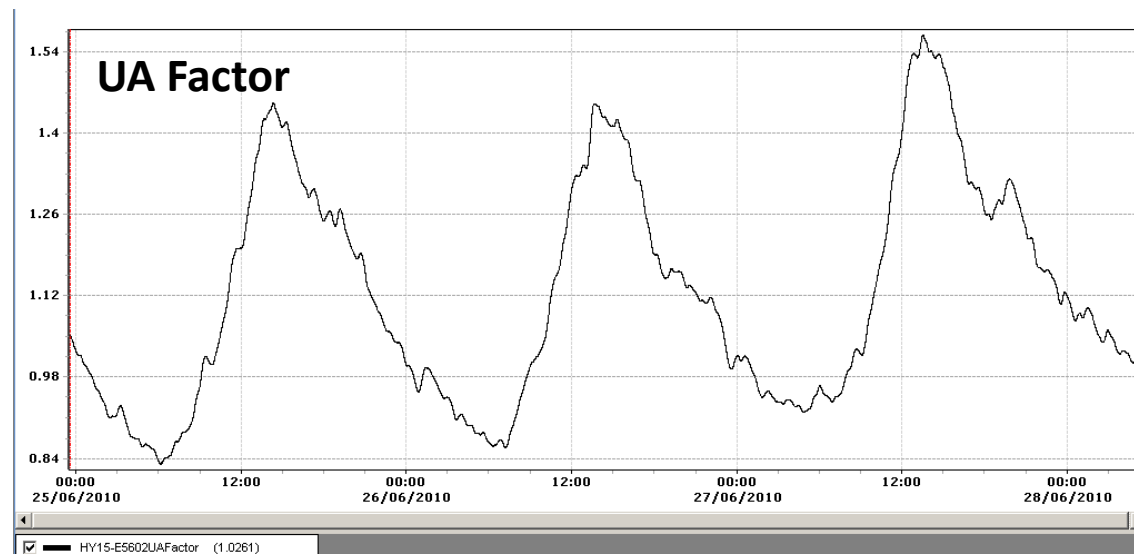


# CW Condenser in HYSYS

The Shell&Tube exchanger of HYSYS Dynamics doesn't consider the effect of shell liquid variations in the heat transfer coefficient.



Therefore a calculated variable UA factor has been introduced in the specified UA of the exchanger. It is a correlation based in pressures and design UAs.



# CW Condensers

It was historically believed that these 6 CW Condensers worked at full capacity all the time with most of the tubes exposed to the hydrocarbons gas.

The HYSYS Dynamics model with a variable UA factor was fitting better with plant data, revealing that **condensers work partially inundated**.

This was effectively verified by the 2-3 Deg C difference between the low shell zone (subcooled) and the high shell zone (equilibrium).



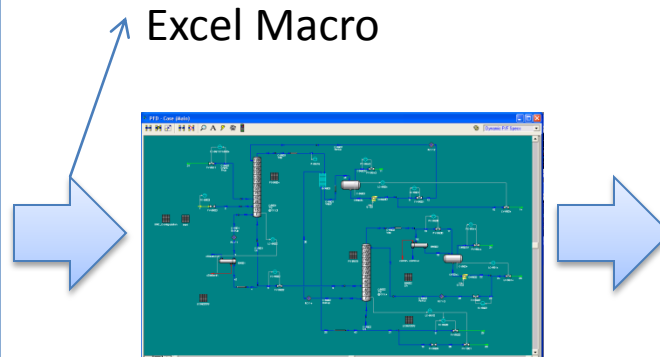


# Validation Method 3:

For 5-days validation period, all the events that occurred in the real plant are synchronically (1 min) introduced into the dynamic model (DMCplus actions, measured disturbances, operators actions) in order to compare the variables calculated by the dynamic model with those obtained from the real plant.

## INPUT DATA :

- Reflux1 (MV1)
- Side-draw (MV2)
- Bottom Flow (MV3)
- Reflux2 (MV4)
- Feed Flow (FF1)
- %C3 Feed (FF2)
- CW Temp. (FF3)
- Feed Temp.
- Steam Temp.
- LC's SP



## OUTPUT DATA :

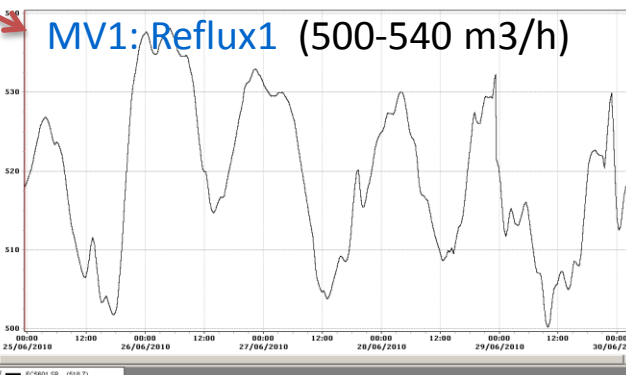
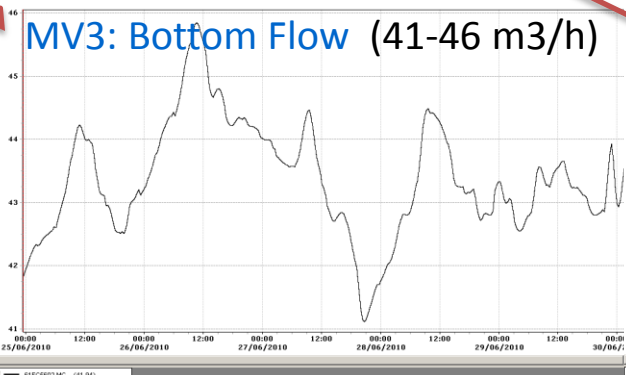
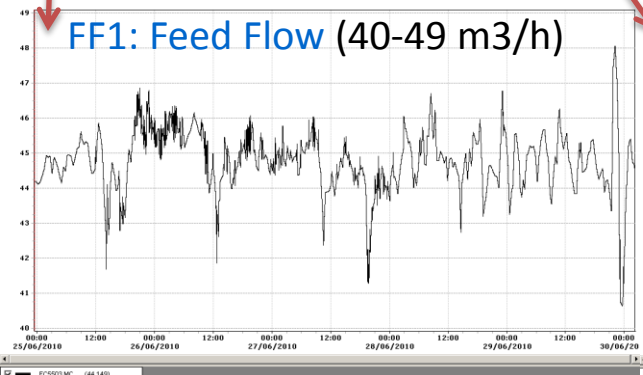
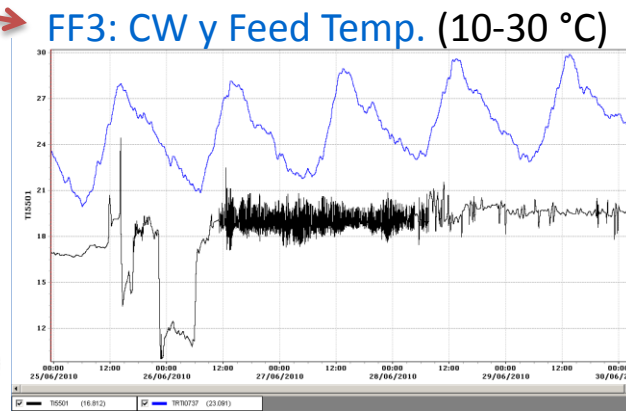
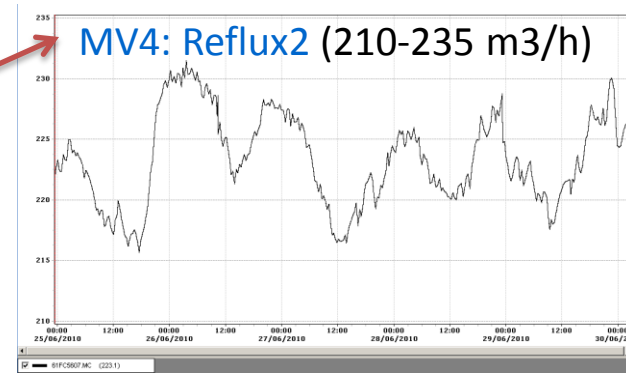
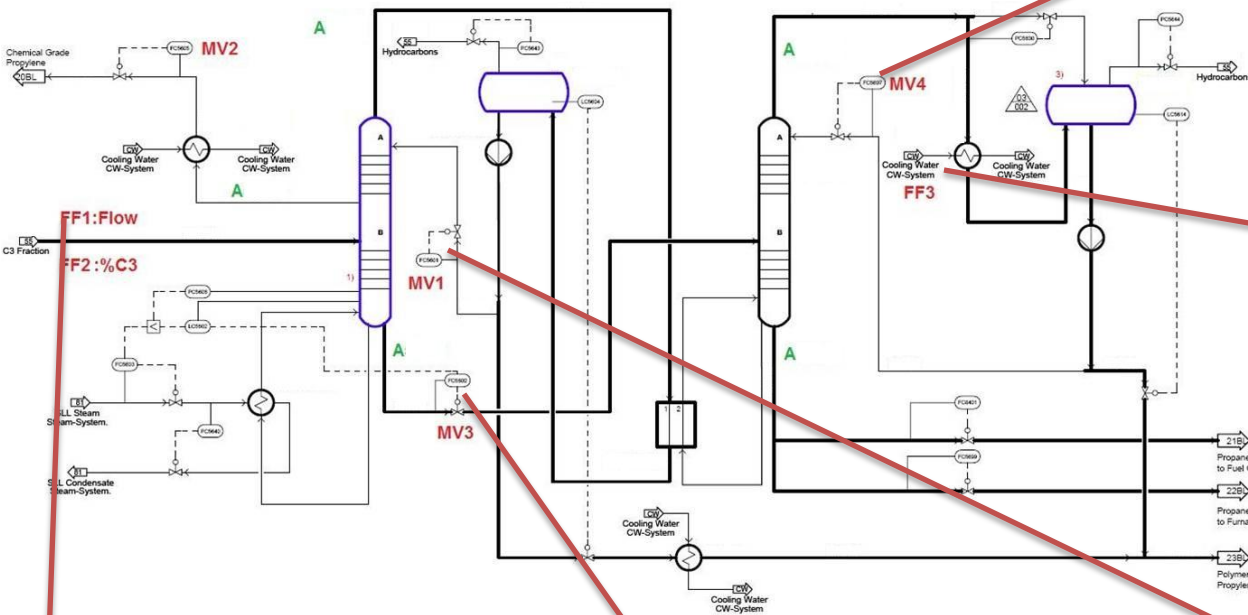
- All compositions
- Temperatures
- Pressures
- Product flows
- etc

This type of validation is only useful if the main disturbances in the real plant are measured, as in the event of there being strong disturbances which go unmeasured they cannot be introduced into the simulation model, with the result that the responses may well be different



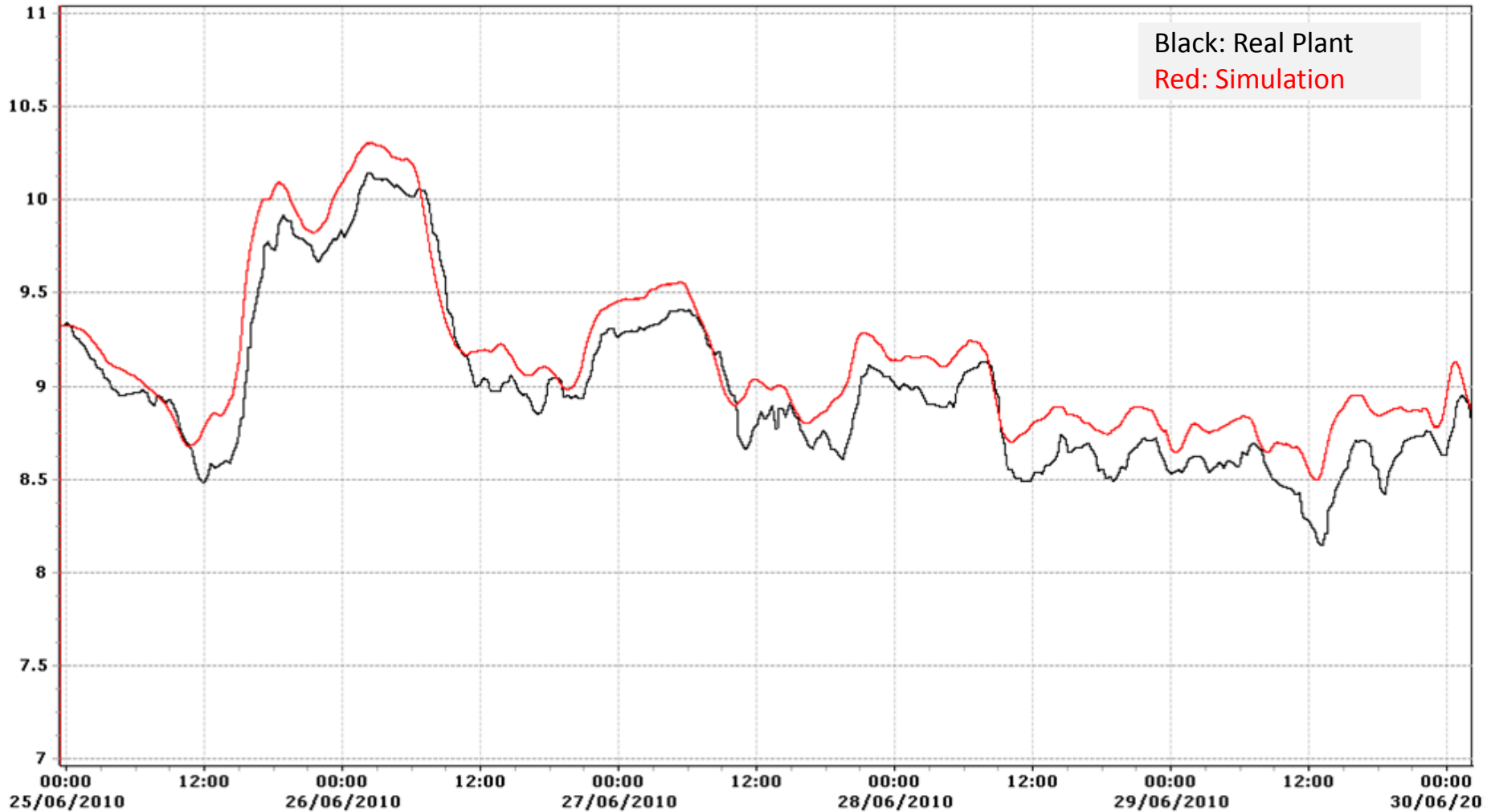
# Some input variables

The DMCplus actions and disturbances were introducing significant changes to the unit



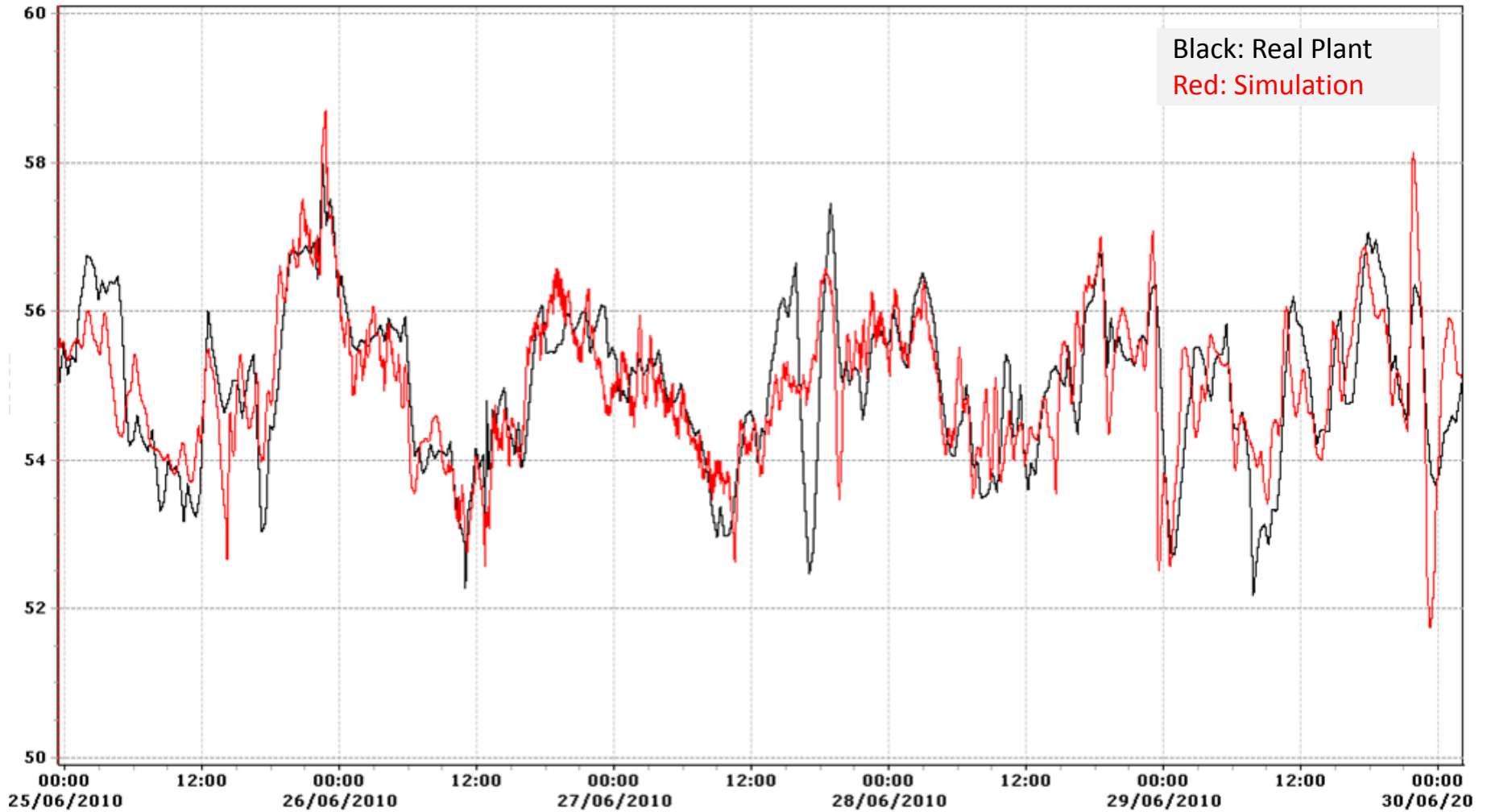
# Validation (Method 3)

1<sup>st</sup> Column Bottom Quality % (C3= in C3)



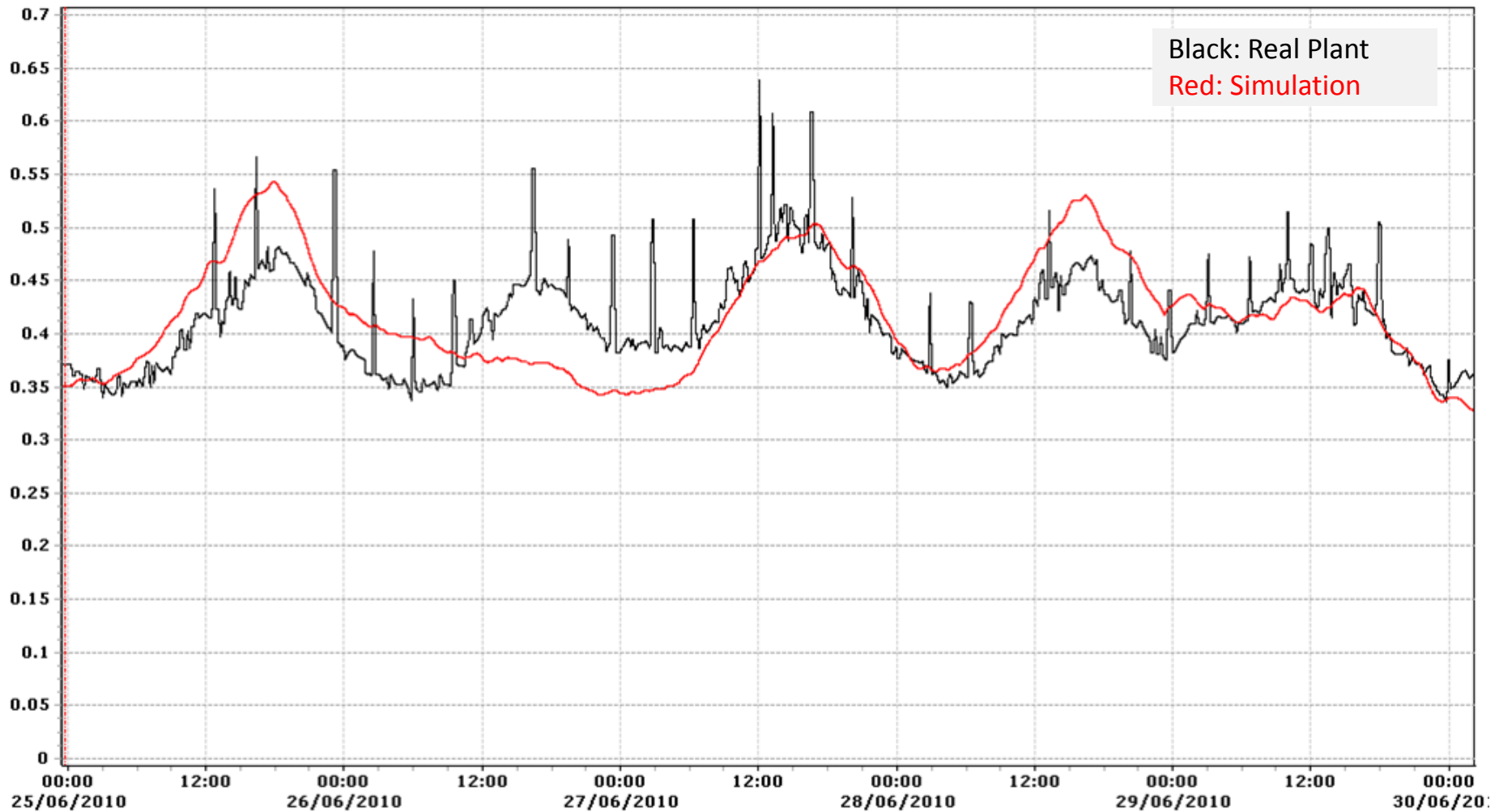
# Validation (Method 3)

1<sup>st</sup> Column Bottom Level (%)



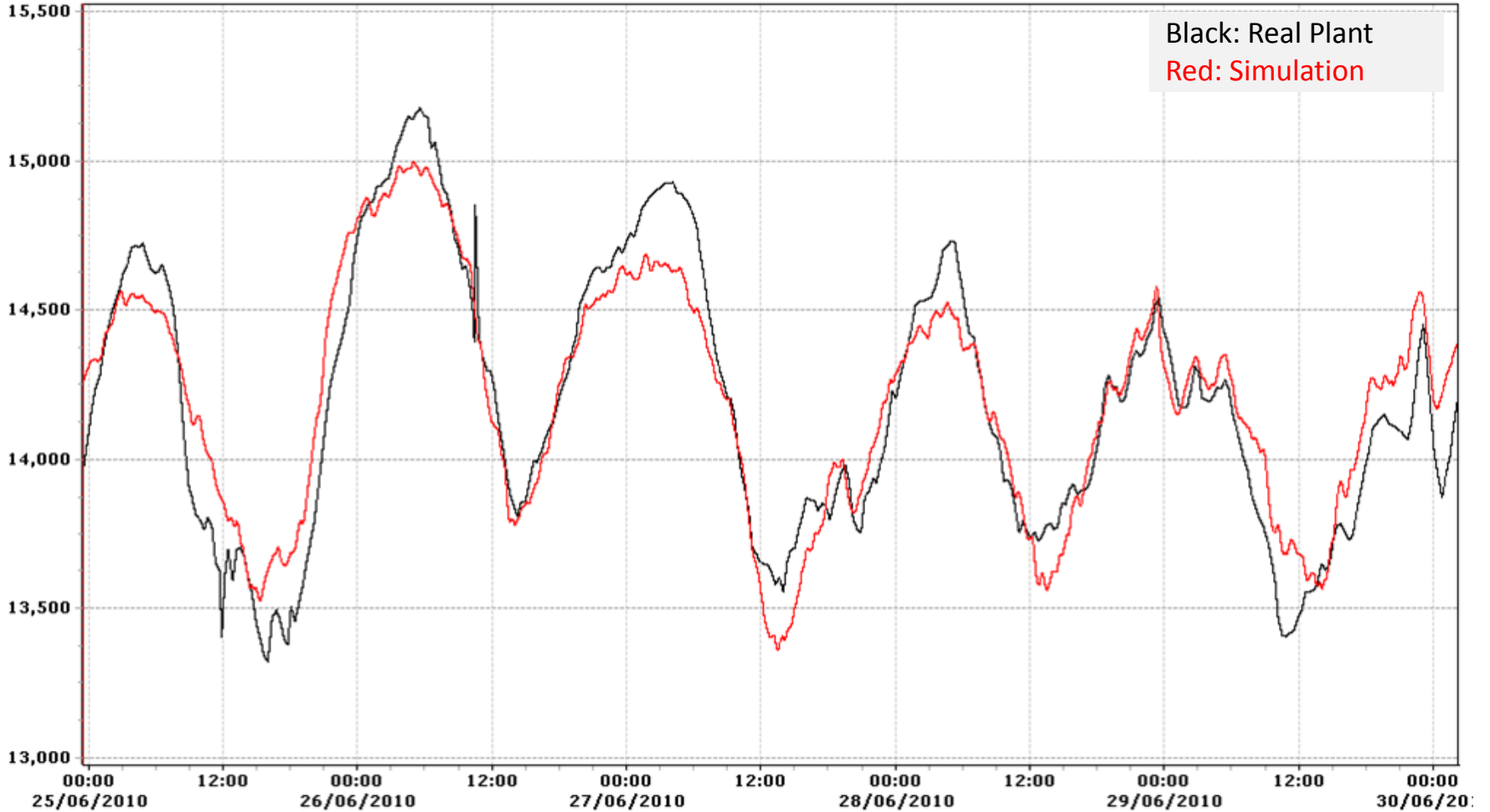
# Validation (Method 3)

2<sup>nd</sup> Column Top Quality % (C3 in C3=). Scale: 0 to 0.7%



# Validation (Method 3)

2<sup>nd</sup> Column Differential Pressure (mbar)

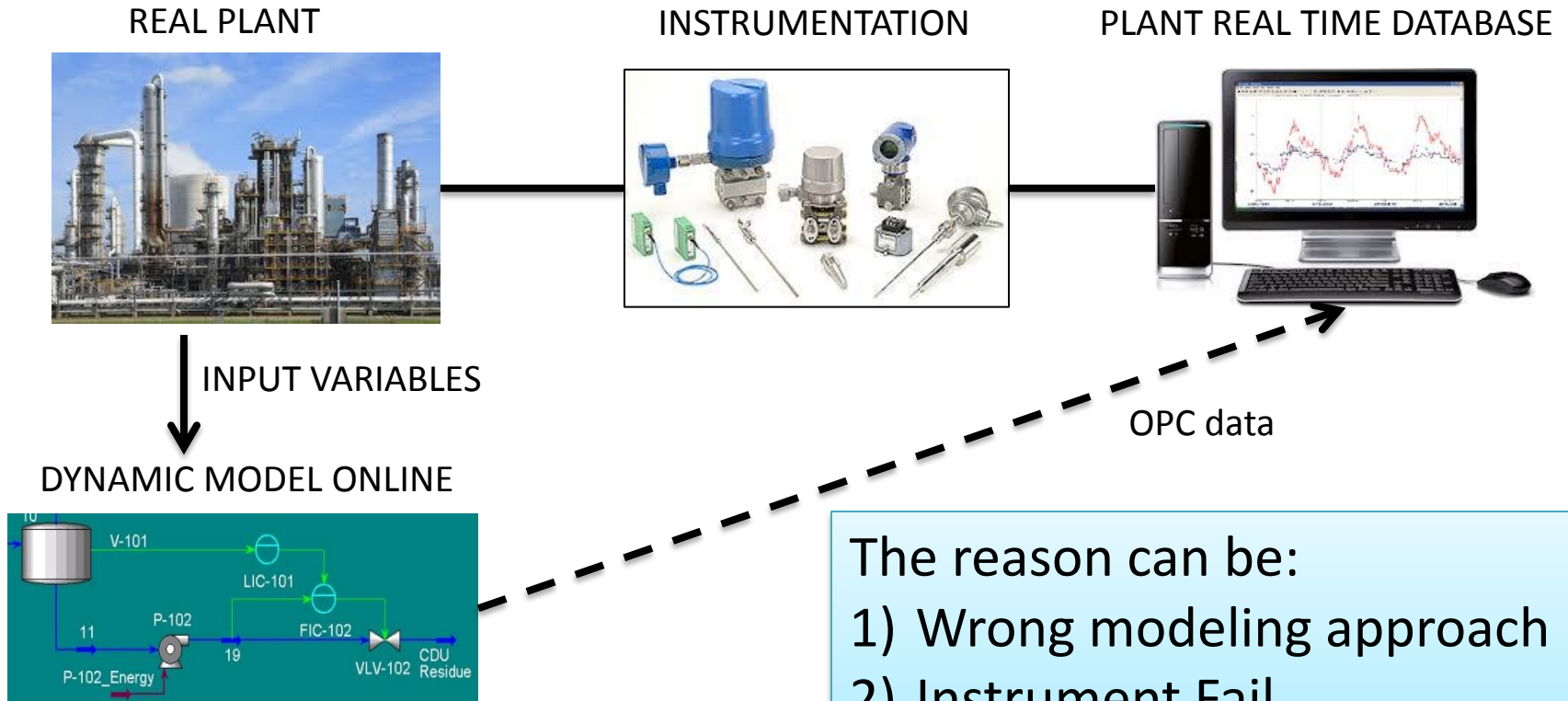


# Ideas for Future: Virtual Sensor

- Steady-state online models need a reconciliation step in order to close Heat & Material balances of imbalanced real plants.
- Dynamic online models would **not need this reconciliation** step, but a proper input variable selection and some self adapted parameters (fouling, efficiencies, etc). Not an obvious task.
- Dynamic online models could provide virtual sensors for compositions, using them as backups of online analyzers which frequently require costly maintenance.
- With online dynamic models, the number and location of the instruments can be revisited, helping to reduce the instrumentation CAPEX.

# Ideas for Future: Fault Detection

- What happens if an online dynamic model suddenly diverge from some plant data?



The reason can be:

- 1) Wrong modeling approach
- 2) Instrument Fail
- 3) Equipment Fail/Constraint

Fortunately physical laws don't lie !

# Ideas for Future: Look-ahead

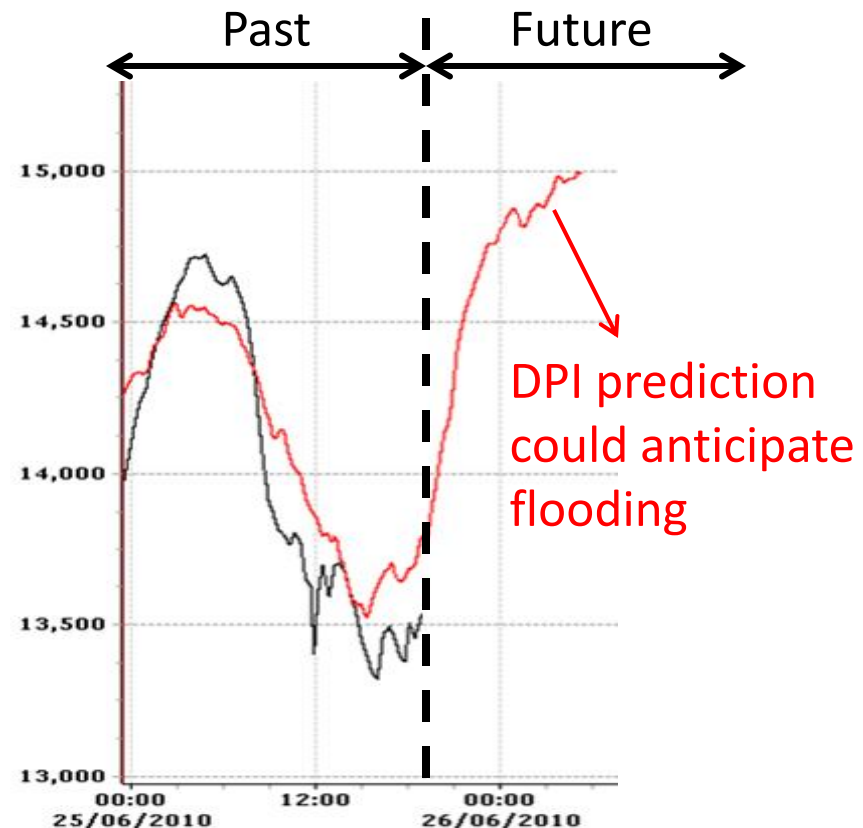


Who does say this?:

*"I've just picked up a fault in the AE-35 unit. It's going to go a hundred percent failure within 72 hours."*



- Online dynamic models can run faster than realtime providing predictions of critical variables
- Realtime look-ahead trends can be combined with plant trending application.

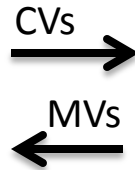




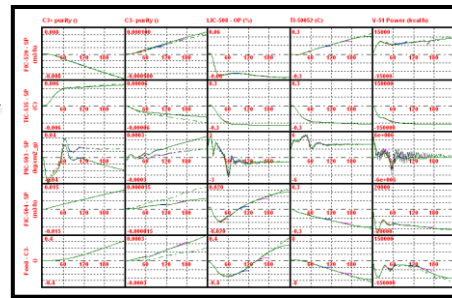
# Ideas for Future: APC

- Look-ahead dynamic model could calculate rigorous CVs predictions, which could replace DMC predictions
- It could be also used as a test bed for DMC tuning

REAL PLANT



DMC1 controller



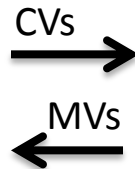
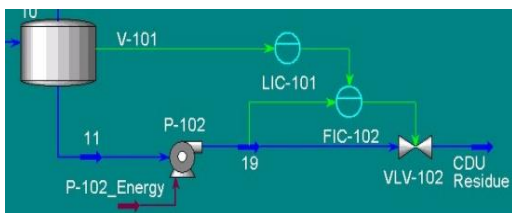
PCWS Interface

Name	Description	Unit	Control	Current Value	Limit	Target	SS	Ustat	Control	External Target	ET Str	ET
ZFL3SEPV	ZFL3SEPV	N	NORMAL	128.007	16.000	121.726	160.000	-8.160				
ZFL3SEPV	ZFL3SEPV	N	SOI LIMIT	19.734	19.000	21.000	20.000	0.027				
ZFL3SEPV	ZFL3SEPV	N	SOI LIMIT	2.200	2.000	2.000	2.000	0.000				
ZFL3SEPV	ZFL3SEPV	N	NORMAL	1.844	1.800	1.960	2.000	0.000				
ZFL3SEPV	ZFL3SEPV	N	NORMAL	69.324	19.000							

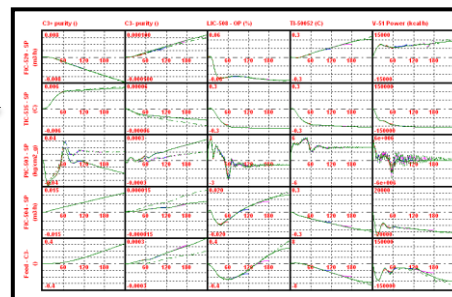
INPUT VARIABLES



DYNAMIC MODEL ONLINE



DMC2 controller



PCWS Interface

Name	Description	Unit	Control	Current Value	Limit	Target	SS	Ustat	Control	External Target	ET Str	ET
ZFL3SEPV	ZFL3SEPV	N	NORMAL	128.007	16.000	121.726	160.000	-8.160				
ZFL3SEPV	ZFL3SEPV	N	SOI LIMIT	19.734	19.000	21.000	20.000	0.027				
ZFL3SEPV	ZFL3SEPV	N	SOI LIMIT	2.200	2.000	2.000	2.000	0.000				
ZFL3SEPV	ZFL3SEPV	N	NORMAL	1.844	1.800	1.960	2.000	0.000				
ZFL3SEPV	ZFL3SEPV	N	NORMAL	69.324	19.000							

# Conclusions

- When the thermodynamic package represent well the components and the main disturbances into the unit are measured, HYSYS Dynamics models can reproduce plant dynamics with acceptable precision and validation method 3 can be used.
- Exploiting the value of such models is still an issue
- Specific education on simulation for non-process engineers is required (Dynamic Simulation for Control Engineers course)
- Some HYSYS Dynamics improvements would be desirable